Equilibrium

Reversible RXⁿ → which proceed in forward as well as in backward direction

Effect of change for any Variable → change in conc of any species in all the...

Point of Eq^m

Features of Equilibrium state of RXⁿ:

① Any property is invariable w.r.t. time

② For RXⁿ at Eq^m

Rate of forward direction = Rate of backward direction

③ For this RXⁿ reaction must be closed

④ RXⁿ is dynamic in nature

⑤ Value of K_c is constant.

At constant parameters (conc, T, P, molar density, colour etc.) become constant for each species present in RXⁿ

Change in conc for any species at Eq^m is 0

⑥ Catalyst equally increase rate of forward and backward direction so that Eq^m is attained faster without changing the K_c value and Eq^m conc (i.e. for $A \rightleftharpoons B$, $K_c = \frac{[B]}{[A]}$, for $A \rightleftharpoons B + C$, $K_c = [B][C]$)

⑦ Eq^m of RXⁿ can be achieved from either direction (forward or backward).

Equilibrium

$R_f = R_b$

Law of chemical Eq^m

$aA(g) + bB(g) \xrightleftharpoons{} cC(g) + dD(g)$

R_f (Rate of forward RXⁿ) $\propto [A]^a [B]^b$

$R_f = k_f [A]^a [B]^b$

similarly $R_b = k_b [C]^c [D]^d$

At Eq^m, $R_f = R_b$

$k_f [A]^a [B]^b = k_b [C]^c [D]^d$

$\frac{k_f}{k_b} = \frac{[C]^c [D]^d}{[A]^a [B]^b}$

$K_c = \frac{[C]^c [D]^d}{[A]^a [B]^b}$

K_c → Equilibrium constant in terms of concentration

K_f → Rate const for forward RXⁿ

K_b → " " " Backward RXⁿ

Conc → molar/molarity (mol/L) for liquid and aqueous species → $\frac{gm}{Molar\ mass}$ for gaseous species

$PV = nRT$

$P = \frac{n}{V} RT$

$P = [X] RT$

$[X] = \frac{P}{RT}$ (Conc of gas species)

K_p → Equilibrium constant in terms of partial pressure

$K_p = \frac{(P_C)^c (P_D)^d}{(P_A)^a (P_B)^b}$

P_C → Partial pressure of C at Eq^m

$P_C = \chi_C P_T$

$P_C = [conc] RT$ → $\propto P$ pressure

$P_A = \chi_A P_T$

$P_B = \chi_B P_T$

$P_D = \chi_D P_T$

Ex: $CaCO_3(s) \rightleftharpoons CaO(s) + CO_2(g)$

$K_p = (P_{CO_2}) = \frac{n_{CO_2} RT}{RT}$ $\quad K_c = [CO_2]$

$K_c = [CO_2] = \frac{n}{RT}$

Ex: $CH_3COOH(aq) + conc$ → dilute on adding water

$K_c = \frac{[CH_3COO^-][H^+]}{[CH_3COOH]}$

Ex: $CH_3COOH(l) + C_2H_5OH(l) \rightleftharpoons CH_3COOC_2H_5(l) + H_2O(l)$

$K_c = \frac{[CH_3COOC_2H_5][H_2O]}{[CH_3COOH][C_2H_5OH]}$

Relation b/w K_p and K_c

$aA(g) + bB(g) \rightleftharpoons cC(g) + dD(g)$

$K_p = \frac{(P_C)^c (P_D)^d}{(P_A)^a (P_B)^b}$ $\quad K_p = [X]^{\Delta n}$

$= \frac{([C]RT)^c ([D]RT)^d}{([A]RT)^a ([B]RT)^b}$

$= K_c (RT)^{(c+d)-(a+b)}$

$K_p = K_c (RT)^{\Delta n}$ → Δn of gaseous species. Conc for gaseous species

Ex: $2NH_3(g) \rightleftharpoons N_2(g) + 3H_2(g)$ $\quad K_p = K_c (RT)^2$

NH_3 → R_2 oxidizing agent

R_2 → reducing agent

$R_2 = \frac{n_2}{n_1}$

(i) $T = \infty K$

$\frac{n_2}{n_1} = 1$

$(RT)^{\Delta n} = 1$

$K_p = K_c$

(ii) $T > \infty K$

$\frac{n_2}{n_1} > 1$

$\left(\frac{n_2}{n_1}\right)^{\Delta n} > 1$, $\Delta n > 0$

$(RT)^{\Delta n} > 1$ → $K_p > K_c$

(iii) $T < \infty K$

$\frac{n_2}{n_1} < 1$

$\left(\frac{n_2}{n_1}\right)^{\Delta n} < 1$, $\Delta n > 0$

$(RT)^{\Delta n} < 1$ → $K_p < K_c$

Ex: (i) $CH_3COOH(aq) + H_2O(l) \rightleftharpoons CH_3COO^-(aq) + H_3O^+(aq)$ → example of heterogeneous Eq^m

$K_c = \frac{[CH_3COO^-][H_3O^+]}{[CH_3COOH][H_2O]}$

(ii) $CH_3COOH(aq) + NaOH(s) \rightleftharpoons CH_3COONa(s) + H_2O(l)$ → example of heterogeneous Eq^m

$K_c = \frac{[CH_3COO^-][Na^+][H_2O]}{[CH_3COOH][NaOH]}$

Factors affecting Eq^m Const (K_{eq})

$K_p(s) = \frac{[P_C]^c [P_D]^d}{[P_A]^a [P_B]^b}$

$K_p = K_p(s) \cdot [P_A]^a [P_B]^b$

$\propto$ if it is Eq^m const.

① Temp

② Mode of Representation of RXⁿ

Representation of RXⁿ → Changes, RXⁿ becomes reverse of the Eq^m conc and Eq^m Const becomes reciprocal

① Temp

K_{eq} and T

(i) $\Delta H = +ve$ (Endo)

$T_2 > T_1$

$T_2 \uparrow$, $K_{eq} \uparrow$

$K_{eq} = f(T)$

(ii) $\Delta H = -ve$ (Exo)

$T_2 > T_1$

$T_2 \uparrow$, $K_{eq} \downarrow$

Rxⁿ when T is high

$T_2 > T_1$ when T is high

(i) $\ln\left(\frac{K_2}{K_1}\right) = \frac{\Delta H}{R}\left[\frac{1}{T_1} - \frac{1}{T_2}\right]$ → as exponential Δ const

$\ln\left(\frac{K_2}{K_1}\right) = \frac{\Delta H}{R}\left[\frac{T_2 - T_1}{T_1 T_2}\right]$

$\ln\left(\frac{K_2}{K_1}\right) = \frac{\Delta H}{R}\left[\frac{\Delta T}{T_1 T_2}\right]$

$K_2 > K_1$ when $\Delta H = +ve$

Slope $= \frac{\Delta H}{R}$

(ii) If K_{eq} of RXⁿ at R removed time at $T_1 \rightarrow K_1$, at $T_2 \rightarrow K_2$, $T_2 > T_1$

$\ln\left(\frac{K_2}{K_1}\right) = \frac{\Delta H}{R}\left[\frac{1}{T_1} - \frac{1}{T_2}\right]$

$\ln\left(\frac{K_2}{K_1}\right) = \frac{\Delta H}{R}\left[\frac{T_2 - T_1}{T_1 T_2}\right]$

② Mode of Representation

(i) Reversal of RXⁿ →

Ex: $A \rightleftharpoons B$; $K_{eq} = \frac{[B]}{[A]} = K_c$

$B \rightleftharpoons A$; $K_{eq} = \frac{[A]}{[B]} = \frac{1}{K_c}$

$K_c = \frac{1}{K_f}$

(ii) Change in Stoichiometric coeffs

$A \rightleftharpoons 2B$ $\quad K_1 = \frac{[B]^2}{[A]}$

$2A \rightleftharpoons B$ $\quad K_2 = \frac{[A]^2}{[B]} = K_1^2$

(iii) Addition of RXⁿ → Eq^m const multiplied

Ex: $A \rightleftharpoons 2B$; $K_1 = \frac{[B]^2}{[A]}$

$2C \rightleftharpoons E$; $K_2 = \frac{[E]}{[C]^2}$

$A + C \rightleftharpoons 2B + E$; $K_3 = \frac{[B]^2 [E]}{[A][C]^2} = K_1 K_2$

Ex: $A \rightleftharpoons B$ $\quad K_1$

$C \rightleftharpoons D$ $\quad K_2$

$A - C \rightleftharpoons B - D$ $\quad K_3$

or

$A + D \rightleftharpoons B + C$ $\quad K_3 = \frac{K_1}{K_2}$

Ex: $N_2(g) + 3H_2(g) \rightleftharpoons 2NH_3(g)$

Scale up → 2 moles of N_2 & 3 moles of H_2 are added → 2L container at Scale up at Eq^m 2 moles of NH_3 is formed. Find K_c of R_2?

$N_2(g) + 3H_2(g) \rightleftharpoons 2NH_3(g)$

Scale up: 2 mol, 3 mol, 0 mol

Eq^m: 2−x, 3−3x, 2x

Vol: 2L, 2L, 2L

Conc: $\frac{2-x}{2}$, $\frac{3-3x}{2}$, $\frac{2x}{2}$

$\frac{2x}{2} = \frac{1}{2}$ → $x = \frac{1}{2}$ mol

Now value of N_2, H_2 at Eq^m

$\left(\frac{3}{2}\right)$ mol, $\left(\frac{3}{2}\right)$ mol, 1 mol

$\left(\frac{3}{4}\right)$ M, $\left(\frac{3}{4}\right)$ M, $\left(\frac{1}{2}\right)$ M

$K_c = \frac{[NH_3]^2}{[N_2][H_2]^3}$

$K_c = \frac{\left(\frac{1}{2}\right)^2}{\left(\frac{3}{4}\right)\left(\frac{3}{4}\right)^3}$

③ K_p, K_c → unitless

Concept of Le-Chatlier's Principle

"It states that if an external stress is applied to a system in Eq^m, the Eq^m for the time being get disturbed as a result system moves in a direction which tends to reduce the external stress and finally a new Eq^m is obtained."

or

If RXⁿ's Eq^m is disturbed by external stress (by changing T, P, V, Conc, or add of inert gas), then RXⁿ shift either forward or Backward RXⁿ to achieve new Eq^m.

① Effect of Change in conc of gaseous or aqueous species

Reactant ↑es, Forward Shift

Product ↑es, Back "

Reactant Removed, Back "

Product " , Forward Shift

② Effect of Pressure & Volume

Piston is pressed downwards, Collision in Reactant Side is increased more than in Product side, So RXⁿ takes place to achieve Eq^m in Forward side.

(i) ↑↑ (V↓), Eq^m shifts towards less no of gaseous molecule side.

P↓ (V↑es) ; " " more n " " "

③ Temp Effect → Only factor to change Eq^m const & Eq^m point.

$A + B \rightleftharpoons C$; $\Delta H = -x$

or

$Ex + A + B \rightleftharpoons C + \Delta H$

$CHE \rightleftharpoons Fe + \Delta H$; $\Delta H = +y$

or

$CHE + \Delta H \rightleftharpoons Fe + H$ pseudo

T ↑es ; Rxn moving from ΔH side

T↓es, Rxn towards ΔH side

Ex: $N_2 + 3H_2 \rightleftharpoons 2NH_3(g)$; $\Delta H = -46.3$ KJ/mole

T low for high to favour the RXⁿ !

Ex: $ESH_2(g) + nO_2(g) \rightarrow nH_2O + SO_2(g)$; $\Delta H = -ve$

To favour the RXⁿ

i) T ↓ ; RXⁿ → low

ii) P ↑ ; RXⁿ → low

(iii) Conc of O_2 ↑ → ✓

Ex: $2NH_3(g) \rightleftharpoons N_2(g) + 3H_2(g)$

& P ↑ ↓ ↑ to favour RXⁿ

No effect of pressure.

④ Add^n of inert gas (Ar, He, Ne, Sometimes N_2, CO_2)

i) At const Volume, No effect of add^n on Eq^m point

ii) At const pressure, Eq^m point shift towards more no of gaseous moles.